

**TITLE: FAST COMPUTATION OF DECISION FEEDBACK EQUALIZER
COEFFICIENTS**

SPECIFICATION

CROSS REFERENCE TO RELATED APPLICATION

5 This application claims priority to U.S. Provisional Application Serial No. 60/322,994,
filed September 18, 2001, which is incorporated herein by reference in its entirety.

1. FIELD OF THE INVENTION

This invention relates generally to digital communications; and more particularly to
decision feedback based equalizers.

2. BACKGROUND OF THE INVENTION

10 The structure and operation of communication systems is generally known. Many
communication systems carry data, e.g., voice, audio, video, file, or other digital data that is sent
from a transmitter to a receiver. On the transmitter side, data is first formed into packets. This
15 data may be raw data or encoded data that represents the raw data. Each of these packets also
typically includes a header, a known training sequence, and a tail. These packets are then
modulated into symbols and the symbols are transmitted by the receiver and intended for receipt
by the receiver. The receiver then receives the symbols and attempt to extract the data from the
packets that are carried by the symbols.

20 A "channel" carries the symbols from the transmitter to the receiver. The channel is
serviced by a wired, wireless, optical, or another media, depending upon the communication
system type. In many communication systems, such as terrestrial based wireless communication
systems, satellite based communication systems, cable based communication systems, etc., the
channel distorts the transmitted symbols, from the perspective of the receiver, causing

interference between a subject symbol and a plurality of symbols surrounding the subject symbol. This type of distortion is referred to as "inter-symbol-interference" and is, generally speaking, the time-dispersed receipt of multiple copies the symbols caused by multipath. The channel also introduces noise into the symbols prior to their receipt. Each of these concepts is well known.

5 Equalizers are now generally employed in an attempt to remove channel effects from a received symbol stream. Thus, equalizers are essential building blocks of modern receivers, especially in broadband applications where inter-symbol-interference is a critical problem. In a typical equalizer, the channel between the transmitter and the receiver is first estimated based upon the training sequence contained in one or more preambles. Then optimal equalizer coefficients (also referred to as taps and/or tap coefficients for the equalizer) are estimated based upon the channel estimate. The optimal equalizer coefficients are then used by the equalizer in extracting the data from the packet. The optimal equalizer coefficients may also be computed after extraction of the data from the equalized data stream based upon blind channel estimates. Equalizer coefficient generation should be repeated as often as possible, especially in fast varying channel cases, to generate new equalizer coefficients. The received data stream is usually buffered during the period that is required for channel estimation and equalizer coefficient computations. Thus, the preamble (and also actual data) contained in a packet may be used to generate the channel estimate and optimal equalizer coefficients that are employed by the equalizer to extract the data from the packet.

20 As symbol rates increase and modulation schemes become more complex, equalizers have increasingly greater importance. A critical factor in increasing the effectiveness of these equalizers is the complexity of optimal equalizer coefficient computation. A reduction in this

complexity: (1) reduces the memory size required to buffer the received symbol stream sequence during the period required for coefficient computations; (2) allows more frequent uploading of new coefficients thus enabling the equalizer to track fast channel variations; and (3) simplifies the hardware and, resultantly, the die area required for coefficient computation.

FIG. 1 is a block diagram illustrating a discrete time symbol-spaced Decision Feedback Equalizer (DFE) based channel equalization model 100. The channel equalization model 100 includes a channel 102, a Feed Forward Equalizer (FFE) 104, a Decision block 106, and a Feed Back Equalizer (FBE) 108. An input sequence $x(n)$ is complex, independent and identically distributed with unit power. Additive noise $v(n)$ is white Gaussian with power spectral density σ_v^2 . Furthermore, the decisions $\hat{x}(n-\delta)$ are assumed to be correct, and hence equal to $x(n-\delta)$. This assumption makes the design of the FBE 108 and FFE 104 easier, but at the expense of introducing error propagation due to possibly wrong decisions. The FFE 104 function $G(z)$ has length L . The channel (impulse) response vector of the channel h is given in Equation (1) as:

$$h = [h(0) \ h(1) \ \dots \ h(N-1)] \quad \text{Equation (1)}$$

The number of coefficients (taps) M of the FBE 108 function $B(z)$ is assumed greater or equal to the channel memory, i.e., $M \geq N-1$. These modeling assumptions are feasible in practice.

In estimating FFE 104 and FBE 108 equalizer coefficients, the goal is to minimize the mean square error quantity of Equation (2).

$$\zeta = E|x(n-\delta) - \hat{x}(n-\delta)|^2, \quad \text{Equation (2)}$$

where $\hat{x}(n-\delta)$ is the delayed input signal estimate prior to the Decision block 106. By collecting the coefficients of both $G(z)$ and $B(z)$ into vectors, we can express the received signal

$\hat{x}(n - \delta)$ in Equation (3) as:

$$x_n = y_n g - \tilde{x}_n b \quad \text{Equation (3)}$$

A channel output model defining y_n may be expressed by:

$$y_n = x_n H + v_n \quad \text{Equation (4)}$$

where H is the $(N + L - 1) \times L$ convolution matrix corresponding to the channel response and expressed as:

$$H = \begin{bmatrix} h(0) & 0 & \cdots & 0 \\ h(1) & h(0) & \cdots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ h(N-1) & h(N-2) & \ddots & h(0) \\ 0 & h(N-1) & \ddots & h(1) \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \cdots & h(N-1) \end{bmatrix} \quad \text{Equation (5)}$$

In this model, x_n is the $1 \times (N + L - 1)$ input vector,

$$x_n \stackrel{\Delta}{=} [x(n) \quad x(n-1) \quad \cdots \quad x(n-N-L+2)] \quad \text{Equation (6)}$$

y_n is the $1 \times L$ input regression vector to the FFE 104,

$$y_n \stackrel{\Delta}{=} [y(n) \quad y(n-1) \quad \cdots \quad x - y(n-L+1)] \quad \text{Equation (7)}$$

\tilde{x}_n is the $1 \times M$ input regression vector to the (strictly causal) FBE 108,

$$\tilde{x}_n \stackrel{\Delta}{=} [x(n-\delta-1) \quad x(n-\delta-2) \quad \cdots \quad x(n-\delta-M)] \quad \text{Equation (8)}$$

and v_n is the $1 \times L$ vector noise process.

The current efficient methods for computing the optimal filter coefficients of a decision feedback equalizer, which optimizes (1), are based on the well-known Cholesky decomposition method (from a finite-dimension problem formulation). Two published papers: (1) N. Al-

Dhahir and J.M. Cioffi, "MMSE Decision-Feedback Equalizers: Finite-Length Results," IEEE Trans. on Information Theory, vol. 41, no. 4, pp. 961-973, July 1995; and (2) N. Al-Dhahir and J.M. Cioffi, "Fast Computation of Channel-Estimate Based Equalizers in Packet Data Transmission," IEEE Trans. on Signal Processing, vol. 43, no. 11, pp. 2462-2473, Nov. 1995

5 provide one procedure for computing optimal DFE settings. These equations are referred to hereinafter as "Al-Dhahir's equations."

Generally speaking, Al-Dhahir's equations, as well as other existent techniques rely on the use of the generalized Schur algorithm for fast Cholesky decomposition of the matrices involved in both the FBE and FFE optimal coefficient setting computations. However, the overall procedures for calculation of the DFE (FBE and FFE) coefficients have the following problems:

1. These procedures require the use of nonstructured recursive equations. These equations are difficult to implement from the perspective of integrated circuit design. In particular, the recursive equations used in Al-Dhahir's DFE tap (coefficient) computer often requires the use of a DSP processor. As is generally known, the use of a DSP processor in a real-time communication system application is severely constricts system throughput.
2. These procedures, in particular Al-Dhahir's equations require a complex tap computer. In other words, they require the use of a relatively large number of complex multiplies.
3. These prior art DFE coefficient computation techniques can be used only for equalizers that use a fixed equalizer delay (δ), which is set to its maximum value $L - 1$, where L is the length of the FFE 104. The prior art techniques cannot use a different delay δ of the equalizer.

Thus, there is a need in the art for a new equalizer coefficient computation methodology

and system in which such methodology may be implemented.

SUMMARY OF THE INVENTION

10 In order to overcome the above-cited shortcomings, among others of the prior art, the
5 method and system of the present invention computes optimal Decision Feedback Equalizer
(DFE) coefficients $\{g_{opt}, b_{opt}\}$ from a channel estimate h . As contrasted to the prior art, the
methodology of the present invention relies on iterating simple structured recursions to yield the
DFE coefficients. Resultantly, the operation according to the present invention produces DFE
coefficients faster and with less computational requirements than the prior art operations, thus
providing significant advantages over prior techniques.

15 According to the present invention, a channel impulse response h is first estimated based
upon either a known training sequence or an unknown sequence. A solution to the DFE
coefficient computation problem is then cast as a standard recursive least squares (RLS) problem.
More specifically, the solution for Feed Forward Equalizer (FFE) coefficients g_{opt} (of the DFE)
based upon the channel impulse response h is formulated as the Kalman gain solution to the RLS
problem. A fast recursive method for computing the Kalman gain is then directly used to
compute g_{opt} .

20 In one embodiment of the present invention, a fast transversal filter (FTF) technique is
employed to compute g_{opt} . In this embodiment, the complexity of a conventional FTF algorithm
is reduced to one third of its original complexity by choosing the length of Feed Back Equalizer
(FBE) coefficients b_{opt} (of the DFE) to force the FTF algorithm to use a lower triangular matrix.

This technique significantly reduces the needed recursions and computations, as well as avoiding finite precision problems of a conventional FTF solution implemented in hardware.

Finally, with the FFE coefficients g_{opt} determined, the FBE coefficients b_{opt} are computed by convolving the FFE coefficients g_{opt} with the channel impulse response h . In performing this operation, a convolution matrix that characterizes the channel impulse response h is extended to a bigger circulant matrix. With the extended circulant matrix structure, the convolution of the FFE coefficients g_{opt} with the channel impulse response h may be performed the convolution operations in a transformed domain. In one embodiment, the convolution is performed in the frequency domain, which can be computed efficiently using the Fast Fourier Transform (FFT). However, in other embodiments, other transformation domains are employed for the convolution operations, e.g., Discrete Cosine Transformation domain and the Discrete Hadamard Transform domain, among others.

The method of the present invention is exact and is much faster than any prior technique that may have been employed to compute DFE coefficients for the same channel and DFE filter lengths. Because the method of the present invention relies upon simple structured recursion, the computation period and/or the hardware required for the DFE coefficient computations is significantly reduced as compared to prior art implementations. The reduction in computation complexity and resultant increase in computation speed enables a DFE that operates according to the present invention to track fast channel variations.

The method of the preset invention may be efficiently used in many communication systems that require the use of equalizers such as mobile wireless receivers, fixed wireless receivers, cable modem receivers, HDTV receivers, etc. to increase the performance of such

communication systems. Other features and advantages of the present invention will become apparent from the following detailed description of the invention made with reference to the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

These and other features, aspects and advantages of the present invention will be more fully understood when considered with respect to the following detailed description, appended claims and accompanying drawings wherein:

FIG. 1 is a block diagram illustrating a discrete time symbol-spaced Decision Feedback Equalizer (DFE) channel equalization model 100;

FIG. 2 is a logic diagram generally illustrating operation according to the present invention in determining DFE coefficients and applying such coefficients to a DFE;

FIG. 3 is a logic diagram illustrating operations according to the present invention employed to determine Feed Forward Equalizer (FFE) coefficients for the DFE;

FIG. 4 is a logic diagram illustrating operations according to the present invention employed to determine Feed Back Equalizer (FBE) coefficients for the DFE;

FIG. 5 is a block diagram illustrating a discrete time fractionally-spaced DFE that operates according to the present invention;

FIG. 6 is a block diagram illustrating a multi-channel equivalent of the discrete time fractionally-spaced DFE of FIG. 5; and

FIG. 7 is a block diagram illustrating a transceiver constructed according to the present invention.

DETAILED DESCRIPTION OF THE INVENTION

FIG. 2 is a logic diagram generally illustrating operation according to the present invention in determining Decision Feedback Equalizer (DFE) coefficients and in applying such coefficients to a DFE. The operations of the present invention are performed by a processor, such as a Digital Signal Processor (DSP), or other circuitry present within a receiver that determines DFE coefficients to be applied to a DFE, also resident in the receiver. The DFE operates upon samples of a received signal in an attempt to remove channel effects from the samples so that digital data may be extracted from the samples. The structure and operation of DFEs, one of which was illustrated in FIG. 1, are generally known and will not be further described herein except as they relate to the present invention.

The operations of the present invention will be first performed by a processor, tap computer, DSP, or other receiver device, to determine initial DFE coefficients to be used in subsequent operations by the receiver. Thus, during startup or reset, a channel corresponding to the receiver is estimated (step 202). According to one embodiment of the present invention, the channel is estimated based upon a known preamble sequence. However, in other embodiments, the channel could also be estimated based upon unknown received data. In either case, channel estimation operations are generally well known and are not described further herein except as it relates to the present invention.

With the channel estimated, Feed Forward Equalizer (FFE) coefficients are determined based upon the channel estimate (step 206). Then, Feed Back Equalizer (FBE) coefficients are determined based upon the FFE coefficients and the channel estimate (step 208). The manner in which the FFE and FBE coefficients are generated is step 206 and step 208 will be described in

detail herein with reference to FIGs. 3-7.

With the FFE and FBE coefficients determined, they are applied to the DFE (step 208) and are used in equalizing samples of a received signal to remove channel effects. These DFE coefficients are continually updated (step 210) using a known technique. Periodically, upon the receipt of a next packet for example, upon an indication that redetermination is required, or upon another triggering event, the DFE coefficients are redetermined (step 212). In this event, another channel estimate may be obtained (step 214). Then, the DFE coefficients are again determined according to the present invention and applied to the DFE. The operations of FIG. 2 continue until the receiver is turned off, placed in a sleep mode, or otherwise inactivated.

FIG. 3 is a logic diagram illustrating operations according to the present invention employed to determine Feed Forward Equalizer (FFE) coefficients for the DFE. In a first operation of FIG. 3, a DFE delay is selected (step 302). In one embodiment, this delay is selected as the channel length. In such case, the DFE delay corresponds to the length of the FFE.

Next, the DFE solution is formulated into a least squares solution (step 304). By collecting the FFE coefficients g and the FBE coefficients b into a single vector w , the minimization of the Mean Square Error may be written as:

$$\min_w E \left| x(n-\delta) - \underbrace{[y_n - \tilde{x}_n]}_u \underbrace{\begin{bmatrix} g \\ b \end{bmatrix}}_w \right|^2 \quad \text{Equation (9)}$$

Now, denoting R_u the variance of the augmented input regression vector u , and cross variance $R_{ux(n-\delta)}$, the well-known solution to this smoothing problem is given by Equation (10) as:

$$w_{opt} = R_u^{-1} R_{ux(n-\delta)} \quad \text{Equation (10)}$$

where

$$R_u \stackrel{\Delta}{=} E \begin{bmatrix} y_n^* \\ -\tilde{x}_n^* \end{bmatrix} \begin{bmatrix} y_n - \tilde{x}_n \end{bmatrix} = \begin{bmatrix} R_y & -R_{y\tilde{x}} \\ -R_{\tilde{y}x} & R_{\tilde{x}} \end{bmatrix} \quad \text{Equation (11)}$$

and

$$R_{ux(n-\delta)} = \begin{bmatrix} E y_n^* x(n-\delta) \\ E \tilde{x}_n^* x(n-\delta) \end{bmatrix} = \begin{bmatrix} R_{yx(n-\delta)} \\ R_{\tilde{x}x(n-\delta)} \end{bmatrix} \quad \text{Equation (12)}$$

Using the channel output model of Equation (4), and the fact that $x(n)$ is individually identically distributed (i.i.d.), the following closed form expressions for $\{R_y, R_{y\tilde{x}}, R_{\tilde{x}}, R_{yx(n-\delta)}, R_{\tilde{x}x(n-\delta)}\}$ are determined:

$$R_y = E y_n^* y_n = \sigma_v^2 I + H^* H \quad \text{Equation (13)}$$

$$R_{y\tilde{x}} = H^* (E x_n^* \tilde{x}_n) = H^* \begin{bmatrix} 0_{(\delta+1)*M} \\ I_M \\ 0_{(N+L-M-\delta)*M} \end{bmatrix} \stackrel{\Delta}{=} \bar{H}^*, \quad \text{Equation (14)}$$

$$R_{\tilde{x}} = I_M \quad \text{Equation (15)}$$

$$R_{yx(n-\delta)} = H^* E x_n^* x(n-\delta) = H^* \begin{bmatrix} 0_{1 \times \delta} & 1 & 0 \end{bmatrix}^T \stackrel{\Delta}{=} h^* \quad \text{Equation (16)}$$

$$R_{\tilde{x}x(n-\delta)} = 0 \quad \text{Equation (17)}$$

where \bar{H} is a submatrix of H as set forth in Equation (5),

$$H = \begin{bmatrix} H_1 \\ \bar{H} \\ H_2 \end{bmatrix} \quad \text{Equation (18)}$$

H_1 is defined as the $(\delta+1) \times L$ submatrix of H , consisting of the first $(\delta+1)$ rows of H . Note that for the case of colored noise, the matrix $\sigma_v^2 I$ should be replaced by the autocorrelation matrix of the noise R_v . Extending the derivation to the colored noise case is straightforward.

5 Now, with the quantities defined above, Equation (10) becomes:

$$w_{opt} = \begin{bmatrix} \sigma_v^2 I + H^* H & -\bar{H}^* \\ -\bar{H} & I \end{bmatrix}^{-1} \begin{bmatrix} h^* \\ 0 \end{bmatrix} \quad \text{Equation (19)}$$

Using the well known inverse formula of block matrices, w_{opt} may be rewritten as:

$$w_{opt} = \left(\begin{bmatrix} 0 & 0 \\ 0 & I \end{bmatrix} + \begin{bmatrix} I \\ \bar{H} \end{bmatrix} (\sigma_v^2 I + H^* H - \bar{H}^* \bar{H})^{-1} \begin{bmatrix} I & \bar{H} \end{bmatrix} \right) \begin{bmatrix} h^* \\ 0 \end{bmatrix} \quad \text{Equation (20)}$$

and as:

$$= \begin{bmatrix} I \\ \bar{H} \end{bmatrix} (\sigma_v^2 I + H_1^* H_1 + H_2^* H_2)^{-1} h^* \quad \text{Equation (21)}$$

which may be written as:

$$\begin{bmatrix} g_{opt} \\ b_{opt} \end{bmatrix} = \begin{bmatrix} I \\ \bar{H} \end{bmatrix} \left(\sigma_v^2 I + \begin{bmatrix} H_1^* & H_2^* \end{bmatrix} \begin{bmatrix} H_1 \\ H_2 \end{bmatrix} \right)^{-1} h^* \quad \text{Equation (22)}$$

20 Although each of the two matrices H_1 and H_2 has a shift structure, the augmented matrix

$\begin{bmatrix} H_1 \\ H_2 \end{bmatrix}$ does not have a shift structure.

In selecting the length of the FBE (DFE delay) to be $M \geq N-1$, the quantities h_δ , H_1 and

H_2 are such that:

$$\begin{bmatrix} H_1 \\ H_2 \end{bmatrix} = \begin{bmatrix} H_\delta & 0 \\ 0 & \tilde{H} \end{bmatrix} \quad \text{Equation (23)}$$

and

$$h = [h_\delta \quad 0] \quad \text{Equation (24)}$$

This implies that:

$$\sigma_v^2 I + H_1^* H_1 + H_2^* H_2 = \begin{bmatrix} \sigma_v^2 I + H_\delta^* H_\delta & 0 \\ 0 & \sigma_v^2 I + \tilde{H}^* \tilde{H} \end{bmatrix} \quad \text{Equation (25)}$$

is block diagonal. In this case, the expressions for g_{opt} and b_{opt} decouple into a simple form.

Therefore, the optimal FFE and FBE coefficients are represented as:

$$g_{opt} = (\sigma_v^2 I + H_\delta^* H_\delta)^{-1} h_\delta^* \quad \text{Equation (26)}$$

$$b_{opt} = \bar{H} g_{opt} \quad \text{Equation (27)}$$

The above expressions are valid for all values of the DFE delay δ . In general, the optimal value for the DFE delay δ is within the range $L-1 \leq \delta_{opt} \leq N+L-2$. In the special case of the choice $\delta = L-1$, the matrices involved in the above expressions are given by

$$H_\delta = \begin{bmatrix} h(0) & 0 & \cdots & 0 \\ h(1) & h(0) & \cdots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ h(N-1) & h(N-2) & \ddots & h(0) \end{bmatrix}, \quad h_\delta^* = \begin{bmatrix} h^*(N-1) \\ h^*(N-2) \\ \vdots \\ h^*(0) \end{bmatrix} \quad \text{Equation (28)}$$

and

$$\bar{H} = \begin{bmatrix} 0 & h(N-1) & \ddots & h(1) \\ 0 & 0 & \ddots & h(2) \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \cdots & h(N-1) \end{bmatrix} \quad \text{Equation (29)}$$

Note that this solution is equivalent to the solution of Al-Dhahir's equations, due to the uniqueness of w_{opt} when Equation (2) is minimized. However, the expressions obtained above for Equations (26) and (27) provide alternative methods to compute the FFE and FBE coefficients g_{opt} and b_{opt} in a simpler and more efficient way than the prior art techniques.

In calculating g_{opt} , a coefficient matrix is first defined in Equation (30) as:

$$P_{\delta}^{\Delta} = (\sigma_v^2 I + H_{\delta}^* H_{\delta})^{-1} \quad \text{Equation (30)}$$

so that the optimal solution for the FFE coefficients g_{opt} is given by

$$g_{opt} = P_{\delta} h_{\delta}^* . \quad \text{Equation (31)}$$

The expression for g_{opt} corresponds exactly to the definition of the Kalman gain vector, used to update the optimal weights in a certain regularized Recursive Least Squares (RLS) problem. More specifically, given a $(n+1) \times L$ data matrix H_n and the corresponding coefficient matrix P_n , the Kalman gain $g_n = P_n h_n^*$ can be time-updated according to the following recursions:

$$\gamma^{-1}(n) = 1 + h_n P_{n-1} h_n^* , \quad \text{Equation (32)}$$

$$g_n = P_{n-1} h_n^* \gamma(n) , \quad \text{Equation (33)}$$

$$P_n = P_{n-1} - g_n \gamma^{-1}(n) g_n^* , \quad \text{Equation (34)}$$

where $P_{-1} = \sigma_v^{-2} I$ (the term P_{-1} is the initial condition for P_n) and $g_0 = 0$. The computation of the Kalman gain vector g_{n+1} in the above solution relies on the propagation of the Riccati variable P_n . This method of computation requires $O(L^2)$ operations per iteration.

Well known fast RLS schemes avoid the propagation of P_n and compute the gain g_n in a more efficient way. In this case, the computational complexity required is only of $\mathcal{O}(L)$ per iteration. This implies that the overall complexity needed to calculate the FFE coefficients can be on the order of $\mathcal{O}(L^2)$ thus yielding an efficient method for computing the FFE coefficients.

Therefore, fast RLS filters are used to determine g_{opt} . In such case, fast transversal computations are employed to determine the Kalman gain for the RLS solution (step 306). Here we also note that it is straightforward to extend this method to use other fast RLS algorithms, e.g., array form fast RLS algorithms.

Faster recursions may be obtained by selecting the FBE length. Such selection eliminates certain variables that remain constant and equal to zero during adaptations in the special solution for g_{opt} . Fast RLS recursion in its explicit form propagates g_n in an efficient manner, see, e.g.: [1] Ljung, M. Morf, and D. Falconer, "Fast calculation of gain matrices for recursive estimation schemes," Int. J. Contr. vol. 27, pp. 1-19, Jan 1978); [2] G. Carayannis, D. Manolakis, and N. Kalouptsidis, "A fast sequential algorithm for least squares filtering and prediction," IEEE Trans. on Acoustic., Speech, Signal Proc., vol. ASSP-31, pp. 1394-1402, December 1983; and [3] J. Cioffi and T. Kailath, "Fast recursive-least-squares transversal filters for adaptive filtering," IEEE Trans. on Acoust., Speech Signal Processing, vol. ASSP-32, pp. 304-337, April 1984.

Table 1 lists the fast recursions employed in one embodiment for computing the normalized Kalman gain. The additional index included in $k_{L,n}$ and $\gamma_L(n)$ stems from the fact that these quantities admit an order-update relation, instead of time-update.

Initialization	
$\zeta^f(-1) = \zeta^b(0) = \sigma_v^2$	
$w_{-1}^f = w_0^b = k_0 = 0$	
$\gamma_L(0) = 1$	
<i>For $n = 0$ to δ repeat operations (1) to (13):</i>	
(1)	$\alpha_L(n-1) = h(n) - h_{n-1}w_{n-2}^f$
(2)	$f(n-1) = \gamma_L(n-1)\alpha(n-1)$
(3)	$k_{L+1,n-1} = \begin{bmatrix} 0 \\ k_{L,n-1} \end{bmatrix} + \frac{\alpha^*(n-1)}{\zeta^f(n-2)} \begin{bmatrix} 1 \\ -w_{n-2}^f \end{bmatrix}$
(4)	$\zeta^f(n-1) = \zeta^f(n-2) + \alpha^*(n-1)f(n-1)$
(5)	$w_{n-1}^f = w_{n-2}^f + k_{L,n-1}f(n-1)$
(6)	$\gamma_{L+1}(n) = \gamma_L(n-1) \frac{\zeta^f(n-2)}{\zeta^f(n-1)}$
(7)	$v(n) = (\text{last entry of } k_{L+1,n-1})$
(8)	$k_{L,n} = k_{L+1,n-1}(1:L) + v(n)w_{n-1}^b$
(9)	$\beta(n) = \zeta^b(n-1)v^*(n)$
(10)	$\gamma_L(n) = \frac{\gamma_{L+1}(n)}{1 - \gamma_{L+1}(n)\beta_L(n)v_L(n)}$
(11)	$b(n) = \gamma_L(n)\beta_L(n)$
(12)	$\zeta^b(n) = \zeta^b(n-1) + \beta^*(n)b(n)$
(13)	$w_n^b = w_{n-1}^b + k_{L,n}b(n)$
Set $g_{opt} = k_{L,\delta}\gamma_L(\delta)$.	

Table 1: Fast Transversal Computation of the Kalman gain.

The purpose of computing k_n in the well-known FTF algorithm is to use it in the computation of the corresponding optimal least squared solution for the FFE coefficients. Because we are interested only in k_n , the filtering part of the FTF algorithm is not necessary, and does not appear in the algorithm listing.

The quantities $\{w_n^f, w_n^b\}$ are known as the least-squares solutions of the forward and

backward prediction problems of order L , with corresponding residual errors $\{f(n), b(n)\}$. Now, because during the first L iterations, the desired signal for the backward prediction problem is equal to zero, the backward least squares solution w_n^b will be equal to zero. This means that all quantities associated with the backward prediction problems will remain nulls for the first L iterations. Since in our case the optimal solution is achieved exactly at the L -th iteration, we can simply rule out the computation of these quantities from Table 1. These operations correspond to operations (7) and (9) through (13) of Table 1. Note that operation (10) of Table 1 is also eliminated, since $\beta(n) = 0$, which implies $\gamma_L(n) = \gamma_{L+1}(n)$. This means that we can replace operation (6) of Table 1 with:

$$\gamma_L(n) = \gamma_L(n-1) \frac{\zeta^f(n-2)}{\zeta^f(n-1)}, \quad \text{Equation (35)}$$

which can be further simplified since

$$\gamma_L(n) = \frac{\zeta^f(-1)}{\zeta^f(0)} \frac{\zeta^f(0)}{\zeta^f(1)} \dots \frac{\zeta^f(n-2)}{\zeta^f(n-1)} = \frac{\sigma_v^2}{\zeta^f(n-1)} \quad \text{Equation (36)}$$

Moreover, operation (8) of Table 1 becomes simply

$$k_{L,n} = k_{L+1,n-1}(1:L) . \quad \text{Equation (37)}$$

where $(1:L)$ denotes the first L entries of $k_{L+1,n-1}$.

Table 2 illustrates a simplified fast recursion for computing the optimal FFE coefficients

\mathcal{G}_{opt} .

Initialization	
$\zeta^f(-1) = \sigma_v^2$	
$w_{-1}^f = k_{L,0} = 0$	
$\gamma(0) = 1$	
<u>For $n = 0$ to δ repeat operations (1) through (7):</u>	
(1)	$\alpha_L(n-1) = h(n) - h_{n-1}w_{n-2}^f$
(2)	$f(n-1) = \gamma(n-1)\alpha(n-1)$
(3)	$k_{L+1,n-1} = \begin{bmatrix} 0 \\ k_{L,n-1} \end{bmatrix} + \frac{f^*(n-1)}{\sigma_v^2} \begin{bmatrix} 1 \\ -w_{n-2}^f \end{bmatrix}$
(4)	$\zeta^f(n-1) = \zeta^f(n-2) + \alpha^*(n-1)f(n-1)$
(5)	$w_{n-1}^f = w_{n-2}^f + k_{L,n-1}f(n-1)$
(6)	$\gamma(n) = \frac{\sigma_v^2}{\zeta^f(n-1)}$
(7)	$k_{L,n} = k_{L+1,n-1}(1:L)$
Set $g_{opt} = k_{L,\delta}\gamma(\delta)$	

Table 2: Fast Transversal Computation of the FFE coefficients.

With the Kalman gain determined, the FFE coefficients are then determined (step 308). In the recursions of Table 2, the FFE coefficients are determined by setting $g_{opt} = k_{L,\delta}\gamma(\delta)$ when the number of iterations, n , is equal to the DFE delay.

Unlike the conventional weighted FTF algorithm, the above recursions do not face finite precision difficulties for the following reasons. First, by ruling out the equations associated with the backward prediction problem, we are automatically eliminating many of the recursive loops that are responsible for the finite precision difficulties of the full FTF algorithm. Second, these simplified fast recursions have a forgetting factor $\lambda = 1$, which yields finite precision stability.

Third, the simplified algorithm deals with a finite set of data ($\delta + 1$ iterations). This algorithm is then reset, which avoids the accumulation of finite precision errors.

FIG. 4 is a logic diagram illustrating operations according to the present invention employed to determine Feed Back Equalizer (FBE) coefficients for the DFE. The FBE coefficients b_{opt} are determined according to the matrix-vector product of Equation (27). The computation of the feedback filter coefficients simply amounts to convolution of the channel impulse response with g_{opt} . The convolution operation that defines the optimal FBE coefficients in Equation (27) can be computed directly with $LM/2$ multiplications. Alternatively, the operations may also be efficiently performed using well-known fast FFT convolution techniques.

To illustrate such operations, Equation (29) is first rewritten in Equation (38) as:

$$b_{opt} = [I_M \quad 0] \begin{bmatrix} \bar{H} & H_3 \\ H_4 & H_5 \end{bmatrix} \begin{bmatrix} g_{opt} \\ 0 \end{bmatrix}, \quad \text{Equation (38)}$$

The above equality holds true regardless of the values of H_3 , H_4 , or H_5 . Now, if these values are chosen such that the matrix C , defined by:

$$C = \begin{bmatrix} \bar{H} & H_3 \\ H_4 & H_5 \end{bmatrix}. \quad \text{Equation (39)}$$

is a square ($Q \times Q$) circulant matrix, where Q is the smallest power-of-two integer larger than or equal $M + L$. In this case, the matrix C is rewritten in Equation (40) as:

$$C = F^* \Lambda F, \quad \text{Equation (40)}$$

where F is a ($Q \times Q$) FFT matrix and Λ is a diagonal matrix that contains the elements of the FFT of the first row of C . The solution for b_{opt} becomes:

$$b_{opt} = [I_M \quad 0] F^* \Lambda F \begin{bmatrix} g_{opt} \\ 0 \end{bmatrix}, \quad \text{Equation (41)}$$

The complexity of this method is the complexity of obtaining the FFT of two vectors of Q elements of each, the inverse FFT of another Q element vector, and Q complex multiples. Thus the overall complexity is

$$Q + 3Q \log_2(Q). \quad \text{Equation (42)}$$

For the case of a power-of-two channel estimate N , the complexity is

$$2M + 6M \log_2(2M). \quad \text{Equation (43)}$$

Thus, referring again to FIG. 4, in determining the FBE coefficients, the convolutional matrix \bar{H} is first determined (step 402). As was previously described, the matrix \bar{H} may be determined as part of the channel estimation. Then, the convolutional matrix \bar{H} is extended to form the bigger circulant matrix C (step 404). The bigger circulant matrix C is then converted to the Frequency domain (step 406) as are the FFE coefficients (step 408). With both the bigger circulant matrix C and the FFE coefficients in the frequency domain, they are convolved in the frequency domain by simple matrix multiplication (step 410) to produce the FBE coefficients b_{opt} . Finally, the resultant FBE coefficients b_{opt} are then converted to the time domain using inverse FFT operations to produce FBE coefficients b_{opt} in the time domain (step 412). The FBE coefficients b_{opt} are then applied with the FFE coefficients g_{opt} to the DFE (as previously described with reference to FIG. 2).

FIG. 5 is a block diagram illustrating a discrete time fractionally-spaced DFE that operates according to the present invention. FIG. 6 is a block diagram illustrating a multi-

channel equivalent of the discrete time fractionally-spaced DFE of FIG. 5. The approach used for the symbol-spaced model can be easily extended to fractionally spaced models. In this section, we shall derive a fast algorithm for a $T/2$ -spaced equalizer. The fast solution for the general case of faster oversampling factors, say $T/3$, $T/4$, . . . , etc. will then follow simply by inspection of the arguments in this section.

FIGs. 5 and 6 illustrate two equivalent representations for a discrete time model of a $T/2$ -spaced equalizer. FIG. 5 illustrates a DFE 500 in terms of an down sampler and up sampler device, while FIG. 6 illustrates a DFE 600 is a corresponding multichannel representation. Thus, as contrasted to FIG. 1, the DFE 500 of FIG. 5 includes a down sampler 502 and an up sampler 504 that alter the sampling frequency. Further, the DFE 600 of FIG. 6 includes a first channel function 602 having channel estimate h_0 and corresponding noise function $v_0(n)$ and FFE 606 coefficients g_0 . Likewise, the DFE 600 of FIG. 6 also includes a second channel function 604 having channel estimate h_1 and corresponding noise function $v_1(n)$ and FFE 608 coefficients $\{g_0, g_1\}$.

The equivalence between the structures of FIG. 5 and FIG. 6 can be easily verified by writing each of the quantities $\{h, g\}$ and $v(n)$ in terms of their polyphase components, and interchanging their position with the down sampler and the up sampler (see, e.g., P.P. Vaidyanathan, "Multirate Systems and Filter Banks," Prentice Hall, NJ, 1993 and J.R. Treichler, I. Fijalkow, C.R. Johnson, Jr., "Fractionally spaced equalizers," IEEE Signal Processing Magazine, vol. 13, no. 3, May 1996 for details). The quantities $\{h_0, h_1\}$ and $\{g_0, g_1\}$ are the so-called polyphase components of the channel and FFEs, and are denoted by N and L size vectors

$\{h_0, h_1\}$ and $\{g_0, g_1\}$ (see FIG. 6). The noise sequences $\{v_0(n), v_1(n)\}$ are also the even and odd samples of $v(n)$, with powers $2\sigma_v^2$.

A model for the multichannel representation, just like the one for the symbol spaced case in equation (4) may be rewritten by collecting $\{g_0, g_1\}$ into a single vector g' , as:

$$g' = [g_1 \quad g_0] \quad \text{Equation (44)}$$

with the output of the multichannel system given by:

$$[y_{0,n} \quad y_{1,n}] g' \quad \text{Equation (45)}$$

Thus, the following model of Equation (46) works for the input to g' :

$$[y_{0,n} \quad y_{1,n}] = x_n [H_0 \quad H_1] + [v_{0,n} \quad v_{1,n}] \quad \text{Equation (46)}$$

where $\{H_0, H_1\}$ are the convolution matrices associated with the subchannels $\{h_0, h_1\}$. It is more convenient, however, to express the inner product in Equation (45) as a function of the original FFE coefficients vector g , by reordering the entries of g' . In this case, Equation (46) is replaced by:

$$y'_n = x_n H' + v'_n \quad \text{Equation (47)}$$

where

$$H' = \begin{bmatrix} h(1) & h(0) & & & & \\ h(3) & h(2) & h(1) & h(0) & & \\ \vdots & \vdots & h(3) & h(2) & & \\ h(2N-1) & h(2N-2) & \vdots & \vdots & \ddots & h(0) \\ & & h(2N-1) & h(2N-2) & & h(2) \\ & & & & \ddots & \vdots \\ & & & & & h(2N-1) & h(2N-2) \end{bmatrix} \quad \text{Equation (48)}$$

Given this convolution matrix and the noise variance σ_v^2 , the solution for the fractionally space problem is simply given by Equations (26) and (27), with $\{H_\delta, \bar{H}, \sigma_v^2\}$ replaced by $\{H'_\delta, \bar{H}', \sigma_v^2\}$ (similarly to the symbol-spaced case, here we assume $M > N - 1$).

For the symbol-spaced DFE, the shift structure of H_δ implies that $k_{L,n} = k_{L+1,n-1}(1:L)$.

That is, the normalized gain $k_{L,n}$ can be computed fast, by performing the order update of $k_{L,n-1}$ to $k_{L+1,n-1}$, and then retaining the first L entries of $k_{L+1,n-1}$ as $k_{L,n}$. The procedure to derive a fast recursion in the $T/2$ -spaced case follows the same principle. The only difference here is that the data matrix H'_δ has now a double shift structure, in the sense that each row is formed by shifting two samples of the channel at a time. Thus, two successive order updates from $k_{L,n-1}$ to $k_{L+2,n-1}$ are performed and then the first L entries of $k_{L+2,n-1}$ are retained:

$$k_{L,n-1} \rightarrow k_{L+1,n-1} \rightarrow k_{L+2,n-1} \quad \text{Equation (49)}$$

so that

$$k_{L,n} = k_{L+2,n-1}(1:L) \quad \text{Equation (50)}$$

In other words, the resulting algorithm is given by two consecutive forward prediction problems similar to operations (1) through (6) of Table 2 of orders L and $L + 1$, respectively. Table 3 lists the resulting algorithm for the $T/2$ -spaced case.

Initialization	
$\zeta_L^f(-1) = \zeta_{L+1}^f(-1) = 2\sigma_v^2$	
$w_{L,-1}^f = w_{L+1,-1}^f = k_{L,0} = k_{L+1,0} = 0$	
$\gamma_L(0) = \gamma_{L+1}(0) = 1$	
<i>For $n = 0$ to δ repeat operations (I) to (II):</i>	
<i>(I) For $q = L$ to $L+1$ repeat operations (1) to (6):</i>	
(1) $\alpha_q(n-1) = h(2n+q-L+1) - h_{n-1}w_{q,n-2}^f$	
(2) $f_q(n-1) = \gamma_q(n-1)\alpha_q(n-1)$	
(3) $k_{q+1,n-1} = \begin{bmatrix} 0 \\ k_{q,n-1} \end{bmatrix} + \frac{\alpha_q^*(n-1)}{\zeta_q^f(n-2)} \begin{bmatrix} 1 \\ -w_{q,n-2}^f \end{bmatrix}$	
(4) $\zeta_q^f(n-1) = \zeta_q^f(n-2) + \alpha_q^*(n-1)f_q(n-1)$	
(5) $w_{q,n-1}^f = w_{q,n-2}^f + k_{q,n-1}f_q(n-1)$	
(6) $\gamma_{q+1}(n) = \gamma_q(n) \frac{\zeta_q^f(n-2)}{\zeta_q^f(n-1)}$	
<i>(II) $k_{L,n} = k_{L+1,n-1} (1:L)$</i>	
Set $g_{opt} = k_{L,\delta}\gamma_{L+2}(\delta)$	

Table 3: Fast Transversal Computation of FFE coefficients for the $T/2$ -spaced equalizer.

In the general case of a T/S spaced equalizer, the fast DFE tap computation is a straightforward extension of the above algorithm, where q is iterated from L to $(L+S-1)$. However, in the fractionally spaced equalizer, the RLS problem is formulated as a multi-channel problem. In such case, a multi-channel Kalman gain is calculated for the multi-channel RLS problem and the FFE taps are determined therefrom. Note that in the expressions of Table 3, successive order updates are performed.

Now, the optimal FBE taps could now be computed as

$$b_{opt} = \begin{bmatrix} I_M & 0 \end{bmatrix} F^* \Lambda_s (F \otimes I_s) \begin{bmatrix} g_{opt} \\ 0 \end{bmatrix} \quad \text{Equation (51)}$$

where Λ_s is a block diagonal matrix, which satisfies

$$C_s = F_s^* \Lambda_s F_s \quad \text{Equation (52)}$$

where $F_s = F \otimes I_s$ and C_s is a block circulant matrix, which is formed by extending the matrix H in the same manner as in Equation (39). As was the case with the symbol spaced operations described above, the convolution may be performed in a transformed domain, e.g., Frequency Transformation domain, Discrete Cosine Transformation domain and the Discrete Hadamard Transformation domain, among others. In such case a Croniker product may be employed in conjunction with such domain transformation in performing multi-channel convolution in the selected transformed domain.

FIG. 7 is a block diagram illustrating a transceiver constructed according to the present invention. The components of the transceiver 700 are resident in a communications device and are illustrated only generally to show how the operations of the present invention would be accomplished in such a transceiver. The transceiver 700 includes a receiver section 702 and a transmitter section 704 and further includes either a wireless transceiver 706 or a wired transceiver, depending upon the system in which the transceiver 700 is implemented. In the case of a cellular device, RF device, satellite system device, or another wireless implementation, the transceiver 700 includes a wireless transceiver. However, in the case of a cable modem, a LAN device, a home networking device, or another device that couples to a physical media, the transceiver 700 includes a wired transceiver 708. Further, if the present invention is

implemented in a Serializer/Deserializer (SERDES) or similar application, the receiver section 702 and transmitter section 704 may couple to a media without a wired transceiver 708.

Further discussion of the transmitter section 704 and receiver section 702 are in the context of baseband processing. In such case, the receiver section 702 receives a baseband signal from the wireless transceiver 706 (or wired transceiver 708) that is baseband modulated and operates upon the baseband signal to extract data. These operations include determining DFE coefficients according to the present invention and operating upon the baseband signal using the determined DFE coefficients.

The transmitter section 704 receives digital data to be transmitted from a host, codes the digital data into a baseband signal, and passes the baseband signal to the RF transceiver 706. The RF transceiver 706 couples the baseband signal to an RF carrier to create an RF signal and transmits the RF signal to a receiving device across a wireless link.

The receiver section 702 receives a baseband signal that carries coded data from the RF transceiver 706. A Programmable Gain Amplifier (PGA) 712 adjusts the gain of the baseband signal and then provides the gain-adjusted baseband signal to an Analog-to-Digital Converter (ADC) 714 for sampling. The ADC 208 samples the gain adjusted baseband signal at a particular sampling frequency, f_s (that is the symbol clock frequency), to produce samples thereof.

A processor 710 couples to the output of the ADC 714 and analyzes a preamble sequence contained in each received physical layer frame. Based upon the preamble sequence, the processor 710 determines a gain to be applied to portions of the baseband signal corresponding to the data carrying portions of the frame and provides this gain to the PGA 712. Further, the processor 710 may also interact with the optional timing compensation section 716 to

compensate for symbol timing and RF carrier mismatches.

5 The processor 710, based upon the preamble sequence (and based upon actual extracted data in some operations), also determines FFE 104 and FBE 108 coefficients. The manner in which these coefficients are determined was previously described in detail herein. Further, and as was also previously described, the processor 710 may estimate a channel and calculate DFE coefficients based upon unknown but assumed data content. After the processor 710 determines these coefficients, they are applied to the FFE 104 and FBE 108 for subsequent use in extracting data from the baseband signal.

10 The structure described in FIG. 7 may be embodied using various types of circuits formed using various manufacturing processes. For example, in one particular embodiment, the RF transceiver 706 (or wired transceiver 708) is embodied in a first integrated circuit that is coupled to a second integrated circuit that includes the transmitter section 704 and the receiver section 702, among other circuits. In another embodiment, the RF transceiver 706, the transmitter section 704 and the receiver section 702 are all formed on a single monolithic integrated circuit. 15 These integrated circuits may be constructed in CMOS or another semiconductor technology, e.g., PMOS, NMOS, Bipolar, etc.

Further, the receiver section 702 of FIG. 7 may be constructed using various circuit elements/combinations. In one embodiment, all structures past the ADC 714 in the receiver section 702 are embodied using a Digital Signal Processor (DSP) or similar processing device. 20 In another embodiment, dedicated signal path circuitry embodies each of the structural components of the receiver section 702, including the processor 710. While a DSP implementation would provide more flexibility, dedicated signal path circuitry would typically

provide higher performance at a lower cost and with lower power consumption.

The structure and operation of the present invention may be employed in satellite communication systems, satellite television systems, HDTV systems, fixed wireless communication systems, mobile wireless communication systems, cable modem/television communication systems, home networking systems, wireless local area networking systems, 5 wired local area networking systems, and many other types of communication systems. The present invention applies to all types of communication devices in which equalizers are employed to operate upon received signals.

The invention disclosed herein is susceptible to various modifications and alternative forms. Specific embodiments therefore have been shown by way of example in the drawings and detailed description. It should be understood, however, that the drawings and detailed description thereto are not intended to limit the invention to the particular form disclosed, but on the contrary, the invention is to cover all modifications, equivalents and alternatives falling within the spirit and scope of the present invention as defined by the claims.